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DIAGNOSTICS OF GUN BARREL PROPELLANTS

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A preliminary investigation of the applicability of the spontaneous Raman diagnostic technique to the determination of the temperature of the propellant gases in the vicinity of the muzzle of a 20mm gun has been completed. It is concluded that with the proper care, and the correct laser excitation wavelength, flow field diagnostics based on laser light scattering can provide the information desired. Some typical temperature measurements were obtained and are discussed in this report. Methods of improving the accuracy of test data are also described.

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I. INTRODUCTION

This report summarizes the activities performed under the referenced contract. The study program was conducted over a two-year period; therefore, for completeness and continuity the program effort will be reviewed from its inception.

Several problems exist in the use of high performance cannon which require a detailed knowledge of the thermodynamic properties of the propellant gases both within the gun barrel and after they leave the muzzle. These are: (i) the barrel erosion which occurs in tank guns when high performance ammunition is fired; this effect is due to the heat transfer which is related to the propellant gas composition and temperature, (ii) muzzle flash is another serious problem with all guns but is particularly important in artillery weapons; muzzle flash analysis depends on a detailed knowledge of the propellant gas properties as they interact with the surrounding atmosphere, (iii) muzzle blast, or over-pressure, has been observed in both howitzers and 30mm cannon mounted on helicopters, which have an adverse effect on both the gun crews and the surrounding structures. In all of these problems, any proposed solution is completely dependent on having an accurate description of the properties of the propellant gases as they emerge from the gun barrel.

The measurement of the gas properties has, in the past, been limited to internal pressures and barrel surface temperatures. From these, one can infer the gas temperature by making several assumptions regarding the interior ballistics behavior. These tech-

niques, due to their inherent limitations, do not provide the required information which is necessary for an accurate modeling of the propellant behavior. Optical methods such as photography, schlieren, and shadowgraphs provide useful information, however, it is mostly of a qualitative nature. Other diagnostic techniques such as emission absorption spectroscopy and two color pyrometry can provide quantitative data, but it is generally of an integrated nature rather than a pointwise measurement. A diagnostic method which is pointwise, remote, simultaneous and instantaneous, and can provide most of the necessary information described above is the spontaneous laser based Raman scattering method. As is well known, the spontaneous Raman scattering technique (Ref. 1-17) is capable of providing accurate information on concentration of species, gas temperature, and with special acquisition and processing methods, also fluctuation, correlation and cross correlation parameters.

The present investigation has been conducted with the aim of determining the applicability of the laser based Raman technique to the diagnostics of the flow field at the muzzle of a 20mm gun following the passage of the projectile. This has application to both the muzzle flash and the muzzle blast problems. A subsequent study could be performed to obtain measurements within the gun barrel; this would be more applicable to the barrel erosion problem.

II. THE RAMAN EFFECT

The Raman effect is the phenomenon of light scattering from a material medium, whereby the light undergoes a wavelength change and the scattering molecules undergo an energy change in the scattering process. The Raman scattered light has no phase relationship with the incident radiation. Based on quantum theoretical considerations, the incident photons collide elastically or inelastically with the molecules to give Rayleigh and Raman lines, respectively, with the inelastic process much less probable than the elastic. The process of light scattering can be visualized, as the process of abosrption of an incident photon of energy E by a molecule of a given initial state, raising the molecule to a virtual state, from which it immediately returns to a final stationary state emitting a photon of energy equal to the difference in energy between the two stationary states and incident energy E. This is seen graphically in the schematic diagram of Fig. 1, where vibrational and rotational transitions are indicated corresponding to the appropriate vibrational and rotational selection rules which are $\Delta J = 0, \pm 2$ and $\Delta V = \pm 1$. Since the anti-Stokes lines must originate in molecules of higher energy level, which are less abundant at normal temperatures, the anti-Stokes lines would be expected to be much weaker than the Stokes lines. This qualitative description of the Raman effect is obviously very superficial. For a more rigorous and complete discussion of this effect one should consult the cited references.

An inspection of Fig. 1 reveals that the impingement of a photon on a molecule, if Raman active, may result in the excitation of vibrational as well as rotational transitions. Fig. 2 presents an

approximate Raman and Rayleigh scattering response from air illuminated by a Ruby laser. It is evident that the Rayleigh as well as the vibrational spectra have closely associated rotational wings. Since, for our purposes, the vibrational scattering is of direct interest, it is worthwhile to examine the vibrational Raman response. It consists essentially of three branches: (1) the intense Q-branch for which $\Delta J = 0$, (2) the much weaker O-branch for which $\Delta J = 2$, and (3) the S-branch for which $\Delta J = +2$ of approximately the same intensity as the O-branch. The O and S branches are much weaker than the Q-branch and represent only about 1% of the intensity of the Q-branch. They are therefore of minor importance as far as the present applications to fluids are concerned. If a highly dispersive instrument is used, the Q-branch can be resolved into components corresponding to the energy levels characterized by the quantum numbers V = 1,2,3, etc. These, of course, will appear at elevated temperatures, and may therefore be used to determine the fluid temperature; see Fig. 3. Since the orientation of the molecules cannot be fixed in a fluid, the scattering will correspond to an average overall molecular orientation, and the vibrational Raman scattered intensity as derived using the Placzek polarizability theory may be expressed as

$$I_{S,A} = CNI_o \frac{(\nu_o \pm \nu)^4 f(\alpha', \gamma')}{(1-\exp\ [\frac{hc\nu}{kT}])} \qquad (1)$$

From the relative intensity of the Stokes and anti-Stokes lines, taking account of the Boltzmann factor, the temperature is given by

$$T = \frac{hc\nu}{k}\ [\ell n\ \frac{I_s}{I_A} + 4\ell n\ (\frac{\nu_o+\nu}{\nu_o-\nu})\ ]^{-1} \qquad (2)$$

It should be noted that the scattered intensity is proportional to the fourth power of the frequency and to the incident intensity and, of course, to the number density of a given species. It is well-known that the pure rotational Raman spectra appearing near the exciting radiation frequency can be quite intense. However, the very small wavelength separation of the lines, particularly in a mixture of gases, makes the pure rotational spectra very difficult to use for diagnostic purposes as defined here in spite of its stronger signals. The weakness of the Raman scattering technique is its low scattering cross section. Consequently, the signal obtainable is a major factor in determining the applicability of the technique to a given problem. The number of photoelectrons contributing to the signal may be written

$$n_s = E_o N \sigma \ell \Omega \eta_o \eta_g E_p^{-1} \tag{3}$$

where E_p is the energy per photon, η_o is the optical efficiency of the collecting optics, and η_g is the quantum efficiency of the photocathode. The last equation may also be written in terms of an output voltage from a photomultiplier tube across a load R, with a gain G and laser pulse duration t,

$$V_5 = E_o N \sigma \ell \cdot \Omega \eta_o \eta_g \cdot G \cdot eR \cdot (E_p \cdot t)^{-1} \tag{4}$$

where e is the electron charge in coulombs and V_s the signal voltage. The last two equations permit the evaluation of the achievable voltage signal or photon-count in a given situation, if not exactly, at least to a first reasonable approximation. The laser pulse in the above approximation is assumed to have a rectangular shape whereas in actuality the laser pulse generally has a Gaussian distribution in

intensity. The voltage signal or photon count must exceed the signals due to background noise or other disturbing signals if the measurement is to be useful.

At this point it is clear that, in principle at least, instantaneous and simultaneous data for the determination of species concentration and temperature can formally be obtained. The former because the Raman transition takes place in a time of the order of fractions of picoseconds for most Raman active molecules, if illuminated by light in the visible range; and the second because one may record the Stokes and anti-Stokes intensity at the same time, the number of data points only depending on the number of receiving channels one has available. The vibrational Raman system, which permits clear identification of species involved, is generally used. An obvious difficulty in performing Raman intensity measurements is the extremely small equivalent Raman scattering cross section. Typically, this cross section may vary between $10^{-29}cm^2$ and $10^{-31}cm^2$, depending on the molecule under investigation and the frequency of the primary light. Since the frequency dependence is of overriding importance here (fourth power), and is essentially the only parameter which is at the disposal of the experimentalist, one would tend to automatically choose the laser operating at the highest frequency. While this choice might be desirable in one respect, other aspects of this choice might be less favorable as will be discussed later.

The line separation of the resulting Raman spectra is greater for longer wavelength lasers than shorter wavelength sources of primary radiation. This feature may become important in cases where several species are involved and their measurement and resolution are desired, in particular when narrow bandpass filters are contemplated.

Figures 4 and 5 illustrate this problem very clearly, both in terms of concentration measurements of a mixture of gases and the preference of using the ratio of the vibrational Stokes to anti-Stokes intensity for the determination of temperature, as opposed to the rotational spectra. It should also be pointed out that the use of nitrogen laser at the conventional energy (1mj) levels available requires the utilization of photon counting techniques and generally mean values of the measured variables are obtained, while with a Ruby laser, due to its much higher energy (4 joules) per pulse, single pulse operation is possible and therefore instantaneous values can be obtained. The latter is also true for a doubled neodymium yag laser operating at 5320Å available at a repetition rate of 10pps at energy levels in excess of 0.5 joules.

In addition to these pulsed lasers, C-W lasers are being utilized to perform Raman measurements. In particular the argon ion laser operated at 5145Å or 4880Å is very useful in steady state systems where mean concentration and temperature are desired. C-W lasers would, of course, be ideal for time resolved Raman measurements of fluctuating flow fields and combustion systems. However, the available commerical lasers are of insufficient power to provide useful data concerning fluctuating systems.

It is therefore apparent from the above the spontaneous laser Raman scattering has all the desired features of an ideal probe. There are, however, problems associated with this diagnostic method. In discussing the feasibility of diagnostics by means of monitoring the intensity of radiation, and particularly scattered radiation resulting from the Raman effect, one must consider the background radiation which may interfere with the desired signal and render it use-

less. There are a number of sources which may contribute to the undesired background radiation. In order of significance they are: Rayleigh scattering, scattering of the incident beam by viewing port windows, walls and large particles in the flow, Mie scattering, gas particle and surface fluorescence, ambient light, detector dark current, electrical noise, and detector shot noise.

The first two, being of the same frequency as the incident beam and thus spectrally separated from the desired signal, can be filtered out using proper interference filters or spectrographs used for the selection of the desired signals. The fluorescence problem can be a very serious problem. Careful selection of the materials and surface coatings may eliminate this problem. In some cases by proper choice of the primary laser this problem can be avoided. In this respect, the use of a Ruby laser has not caused any significant fluorescent problem in this laboratory. The detector dark current and electrical noise can generally be handled by using photomultiplier coolers, which serve a dual purpose of decreasing the dark current and shielding the photomultiplier from electrical interferences. As far as the shot noise is concerned, this problem must be dealt with at the data processing level.

In general the larger the signal-to-noise ratio the better the system. As has been pointed out,[14] a very convenient parameter to assess the capability of a system is the "feasibility index." This index was defined as $\chi = NL\sigma_0\Omega e$ where N is the number density of the scatterers per cm^3, L is the length of the sample in the direction of the laser beam, σ_0 reference cross section, and Ω and e the solid angle and optical efficiency, respectively. The minimum feasibility index for a 1 joule Ruby laser in a single pulse operation is approx-

imately 10^{-15}. Thus, for a situation where this index is below 10^{-15} a 1 joule single pulse laser would not provide the desired information. An increase in the laser energy or any of the other factors may be necessary. There is, however, a limit on the laser energy one may apply. The laser energy density should be below the breakdown threshold which for Ruby and air appears to be around $10^{10} W/cm^2$.

The choice of the proper method of spectral analysis can be very important. There are basically three methods available: the standard monochromators, interference filters, and Fabry-Perot interferometers. Each has a range of applicability and its positive as well as negative features. The interested reader may consult standard texts or some of the following references.(10), (15), (18)

The detection of the scattered photons of interest is best accomplished by photomultipliers. They are the most sensitive low level light detectors available at present, applicable in the wavelength range from u.v. to near infrared or from about 3-10 thousand Angström wave length. The output of the photomultiplier may be used in one of several ways: (i) as an input to a d.c. amplifier, (ii) as an input to a photon counter, (iii) as an input to a phase sensitive detector, or as a combination or modification of the above basic schemes.

In general photon counting is more accurate than a direct reading of the photomultiplier current. The reasons are: (i) the d.c. level caused by leakage currents of photomultiplier tubes cannot be detected by photon counters, (ii) the statistically varying heights of the detector output pulsers are replaced by standard height pulses, (iii) the photon counting rate can be made insensitive to

power supply voltage fluctuations with proper care. However, at high photon count rates, photon counting may present some difficulties particularly if the detection rate exceeds about 10^7 counts/sec.

Recently a new detection system has been introduced. It offers a number of advantages over photomultiplier tubes. It is supposed to be capable of providing simultaneous measurements of the Raman scattering signals of a multiplicity of species at many spatial points, during a single laser pulse. It would therefore be capable, in conjunction with proper computational facilities, of providing in addition to concentration and temperature, data necessary for the determination of spacial correlation functions. Among the commercial units on the market the OMA2 system appears to be the best both in terms of reliability and operation versatility. Although some of the sensitivity claims for the several detection systems are somewhat overstated relative to the commercially available photomultiplier tubes, it still represents a major advance in the laser scattering diagnostic technology.

III. EXPERIMENTAL FACILITY

Since the primary aim of this study was to determine the feasibility of utilizing the spontaneous Raman effect for the diagnostics of the muzzle flow field, a 20mm gun was set up for the experiments. Although the actual problems occur in much larger caliber guns, it was felt that a 20mm gun was the largest that could be used in a laboratory-type environment. Moreover, the basic flow phenomena in terms of the muzzle flash, overpressure, etc., should be quite similar even in a relatively small bore such as a 20mm gun.

The gun was obtained from BRL and was mounted on a heavy duty steel support embedded in a concrete base. The laser, the firing mechanism, and the data acquisition equipment presently consisting mainly of high-speed oscilloscopes, power supplies and connectors were mounted within a concrete walled control room; an access hole for the laser beam was drilled through the wall to the test chamber. A projectile catcher constructed by BRL and filled with sand was installed approximately 10 feet from the muzzle exit. This provided adequate room for the installation of adjustable telescopes and photomultiplier tubes for the acquisition of the Raman scattered radiation and also for the installation of a shadowgraph system.

Figure 6 provides a schematic diagram of the experimental configuration. As can be seen, the gun has been equipped with four kistler pressure transducers: one near the breach, the second 9-5/16" from the end of the muzzle and, the remaining two transducers 1.5" apart, as seen in Figure 7, in the end "addition" to the muzzle. Three electrostatic probes have also been mounted near the muzzle which, in conjunction with a start-stop time interval counter, can indicate the projectile exit velocity. This velocity can also be

obtained using the two muzzle pressure transducers.

The shadowgraph system consisting of a 4 ft focal length 8" diameter parabolic mirror, a triggerable spark located at the focal point and synchronized with the projectile exit position, a projection screen, and a photographic apparatus permits the acquisition of photographs which provide qualitative information on the flow field observables.

Before describing the laser Raman system, it must be mentioned that after reviewing some of the literature and taking note of some of the difficulties experienced by other investigators who were attempting to use a Ruby laser for the diagnostics of the muzzle exit flow field, it was decided to investigate the radiation spectrum of the projectile plume. For that purpose two types of multichannel spectrum analyzers available at the time in our laboratory were utilized. It was found that the emission spectrum of the flow field behind the projectile was in the near infrared region, overlapping the Raman lines produced by a ruby laser. The emission spectrum was observed to extend over the range from approximately 6000Å to 9000Å. The exact emission lines have not been determined due to some difficulties in calibration of the multichannel analyzers. However, it became obvious that due to the intensity and location of the emission spectrum it would not be prudent to rely exclusively on the spontaneous Raman scattering spectrum excited by a Ruby laser. This spectrum would fall exactly within the emission spectrum of the hot propellant gases following the projectile.

It was therefore decided to utilize a doubler on the Ruby laser; this would shift the Raman spectrum into the region of 3000Å to 4000Å which is well outside the emission spectrum of the propellant gases.

The conversion efficiency of the doubler is approximately 20%; with an initial laser pulse energy of 3 joules at 6943Å, the expected output of the doubler is approximately 600mj. As indicated previously, the Raman scattering intensity is proportional to the incident laser energy and to the fourth power of the incident frequency. It is therefore evident that as far as the scattered intensity is concerned, in spite of an 80% loss in the incident power there will be a gain of about 300% due to the increased frequency. Difficulties in terms of spectral line density as indicated above must be dealt with by using very narrow bandpass filters or very selective spectrometers. Since most of the original ruby laser energy is still available it was decided to utilize it in its original form, as seen in Figure 6. After separating the doubled laser light using a dichroic mirror, the remaining 6943Å laser radiation was directed by a mirror and refocussed at the same point as the 3472Å doubler output. It is thus possible to utilize simultaneously two laser frequencies for the acquisition of the pertinent data. Due to the availability of only two sets of photomultiplier tubes suitable for the two given spectral ranges and the desirability of measuring the temperature, it was decided to concentrate on the measurement of the Stokes and anti-Stokes intensities of nitrogen. To this end each photomultiplier tube was equipped with its own telescope, narrow bandpass filters, and band stop filters. Two photomultipliers were of RCA type 8853 and two of EMI type 9813QA. The former were used for the Stokes and anti-Stokes resulting from the 6943Å incident radiation, the latter from the 3473Å wavelength. The Stokes and anti-Stokes filters for the nitrogen molecules corresponding to the 6943Å incident radiation were centered at 8283Å

and 5976Å, respectively, while the bandpass filters for Stokes and anti-Stokes radiation corresponding to the 3472Å incident radiation were centered at 3776Å and at 3211Å. The mounting planes for the two sets of tubes were 90° to each other to correspond to the respective planes of polarization of the two laser beams.

The tests were initiated by firing the gun using the electrical remote firing device. In order to synchronize the transit of the projectile and the firing of the laser, a pressure transducer was utilized to trigger the laser, through an intermediary time delay and triggering generator system. A second time delay system was used to place the laser pulse at an exact, predetermined position behind the projectile. This delay was adjustable to fractions of a microsecond. The sweeps of the recording oscilloscopes were initiated by the laser itself through the photodiode. The data could be directed either towards the recording oscilloscopes or the data acquisition and processing system, as indicated in Figure 6.

IV. DISCUSSION OF RESULTS

A test is initiated by firing the gun from a remote electrical switch. The laser is triggered by the output of transducer No. 3 (Fig. 7) through a series of delay generators which also initiate the oscilloscopes used to record the pressure of transducers No. 1 and No. 2.

The photodiode indicated in Figure 6 is used to monitor the laser energy as well as to initiate the sweep of the high-speed recording oscilloscopes. Pressure transducer No. 3 also initiates the triggering of the spark system for the shadowgraph.

Figure 8 shows two photographs of three oscilloscopic traces each. The upper trace in each of the photographs indicates the time of the laser firing. The lower two traces represent the pressures of transducers No. 2 and No. 1, respectively. The two photographs represent two separate firings of the gun. From the traces, the maximum pressures measured wave 1200psi and 1000psi for the upper and lower traces, respectively, corresponding to pressure transducers No. 2 and No. 1. Figure 9 represents the Stokes and anti-Stokes intensity of N_2 behind the projectiles as a consequence of the 3472Å primary illumination. While the signals appear to be clean and intense, the subsequent firings indicated the same ratio of Stokes to anti-Stokes as well as the same amplitude, even though the point of measurement relative to the passing of the projectile was changed from test to test. It should be mentioned here that the position of measurement could be adjusted by an appropriate time delay selection of the laser firing with respect to the projectile passing transducer Number 3. Since the muzzle temperature (and hence the ratio of Stokes to anti-Stokes intensity) should vary with time, or with projectile

distance from the muzzle, the lack of dependence of the measured data on the projectile position casts some doubt on the veracity of these measurements. It is believed that some extraneous radiation may have produced these anamolous data. In order to find the source of this radiation and the cause of it, several additional tests were conducted. These tests attempted to confirm or disprove several assumptions made as to the origin of this radiation.

The first assumption was that this radiation was associated with some kind of leakage of incident laser light into the receiving tubes. To test this assumption the laser was fired into the atmosphere without the gun being fired; the firing of the laser indicates a Stokes line corresponding to the nitrogen content of the atmosphere. The anti-Stokes line indicates a negligible signal since the air is at ambient temperature. Figure 10 shows these results which eliminate the possibility of any leakage of incident radiation to the photomultiplier tubes.

The second possibility was that there might still be some radiation from the hot gases behind the projectile in the spectral region corresponding to the doubled ruby (3000-4000Å) in spite of the results obtained from the multichannel spectrum analyzers as indicated previously. To examine this assumption, the gun was fired; however, the laser was not fired. It is evident from examination of Figure 11 that there is no resulting signal. This confirms the previous findings that in this spectral region the emissivity of the propellant gases is negligible.

In order to further check out the operation of the system, the laser was fired into an air-methane flame placed in front of the muzzle and the Stokes and anti-Stokes signals were recorded. The tem-

perature of the flame was found from these signals and it agrees with the temperature as measured with a very thin Platinum-Platinum 10% Rhodium thermocouple. The Stokes and anti-Stokes signals were those of nitrogen using exactly the same focussing, filtering and recording system as shown in Figure 9.

The third possible explanation was that the overwhelming contribution to the undesired signal is Mie scattering. This type of scattering, besides being by far the strongest, is also directional. In order to test this supposition, the filters from one telescope and photomultiplier were changed to the other. This caused the scattering direction to change, producing a large change in the signals. This type of scattering (being of the same wavelength as the incident beam) can be eliminated either by increased filtering or by introducing very selective monochromators.

In order to remove these spurious signals, therefore, several sets of new filters were ordered. The specifications were tightened and consequently their attainment, at a cost compatible with our resources, became almost impossible to secure. What we desired was a filter of a narrow bandpass of 10Å maximum, with a high transmission of at least 50% and a rejection of at least 10^8. Since this was not possible, we decided to utilize at least 2 filters of 10Å bandwidth and what was promised - a rejection of 10^5, in series. This would normally provide a rejection in the stop band of 10^{10}; however, the passband, while narrowed, would lose fifty percent of the transmission. The filters were ordered and,after lengthy delays, were finally delivered. As indicated previously, certain calibration procedures have been followed consisting mainly of measuring the temperature in an air methane flame with a Platinum-platinum 10% Rhodium

thermocouple, and measuring the temperature subsequently at the same point using the Stokes to anti-Stokes ratio of the Raman scattered radiation. This procedure has been followed for the global effect. In addition, each filter has been checked individually and as a series combination using a Carry spectrometer. Here some difficulties were also encountered. While it was possible to determine the transmission at the desired frequency, the determination of the quantitative attenuation at the stop band was impossible. This was due to the systematic behavior of the Carry calibration spectrometer. It could only be determined that each filter's attenuation individually or in series with one another was greater than 10^3.

Since the knowledge of the quantitative value of the attenuation in the stop band is only of academic curiosity and does not affect the temperature measurement as long as it is high enough to stop the undesired interfering radiation, this part of the calibration procedure has not been pursued further.

The most important factor, relating the spectroscopically determined temperature and the thermocouple measured temperature, have been determined in a static flame. This factor includes, besides the transmission and attenuation of each individual filter set, the effect of gain of each of the photomultiplier tubes. A number of tests were run in the gun and some of the results are shown in Fig. 12.

It is evident from this figure that the data, while only preliminary, are absolute and indicative of the local temperature of the exhaust gases from the muzzle at a given instant of time and location behind the projectile. When examining Fig. 12 one must realize that the temperatures as shown represent an instantaneous value at a point in space. For a better statistical average temperature, a

greater number of tests should be obtained. It must be noted that for more reliable statistical averages at least 100 to 200 tests per point should be used. In addition one must consider the fact that none of the test firings are exactly reproducible, due to a number of factors. The propellant charge weight is not exactly equal for each projectile. This can be seen by observing the measured projectile velocity at the muzzle of the gun. For approximately three dozen tests that were run with the same nominal projectile weight and propellant load, the measured velocities varied between 1000fps and 1500fps. The data as presented in Fig. 12, therefore, have been grouped according to velocity. The velocities have been arbitrarily divided into three groups; one in the range between 1000 to 1250 ft/sec., the second group between 1250 and 1350 ft/sec., and the third group from 1350 to 1500 ft/sec. This may be partially responsible for the scattered appearance of the data although there are other factors which are also important. As seen in fig. 12 the temperature of the exhaust gases behind the projectile appear relatively constant up to a distance of about two feet behind the projectile; however, several tests conducted at a larger distance indicated a temperature of the exhaust gases of 400°K or less. Some of the other factors which affect the accuracy of the test data relate to the velocity measurement of the projectile. The electrostatic probes were found to be unreliable due to carbon buildup on their exposed surfaces. The velocity measurements and the triggering mechanism signals were, therefore, obtained from the pressure pulses measured by the transducers mounted in the gun barrel. Spurious data were sometimes generated in this technique by the initial shock, created by the propellant ignition, traveling

through the metallic barrel. The precursor pressure wave preceding the projectile down the barrel was also sufficiently strong to prematurely trigger the test sequence, on occasion. These factors introduce errors in both the velocity measurements and in the determination of the exact projectile location when the laser is fired.

The computation of the temperature also has an inherent error which is estimated to be on the order of $\pm$ 100°K. Since the current test program utilized high speed oscilloscopes to record the data, the temperature was obtained by using the peak intensity of both the Stokes and anti-Stokes signal in the following equation:

$$T(°K) = \frac{3357.8}{\ell n \frac{I_s}{I_A} + 1.30} \tag{5}$$

where I_s is the peak intensity of the Stokes signal and I_A is that of the anti-Stokes signal. The constant in the denominator was obtained from the calibration process and although it may also have an error band associated with it, the present range in measured temperatures are relatively insensitive to this number. The primary source of error is introduced by taking the logarithm of the peak intensity; this assumes that the signal shape is similar for both the Stokes and anti-Stokes which may not always be the case. A more accurate method of obtaining the temperature would be to integrate both signals with respect to time and then use the ratio of the integrated values. In order to accomplish this with any degree of accuracy, the raw data must be recorded as an analog function of time and then integrated by computer for the stretched signal. This could not be done in the present test program since, although the Laser Laboratory at the

Polytechnic has this capability, it would have required long transmission lines between the gun facility and the Laser Laboratory. These lines would attenuate the signals and thereby further decrease the accuracy of the data.

For the present program it was decided, therefore, not to utilize the computer and available software for data acquisition and reduction. It was felt that the oscilloscopes, although providing less accuracy, would permit a more rapid evaluation of the Raman scattering technique in the measurement of muzzle flow temperatures. The results shown in figure 12 indicate that the technique is quite useful in obtaining these measurements.

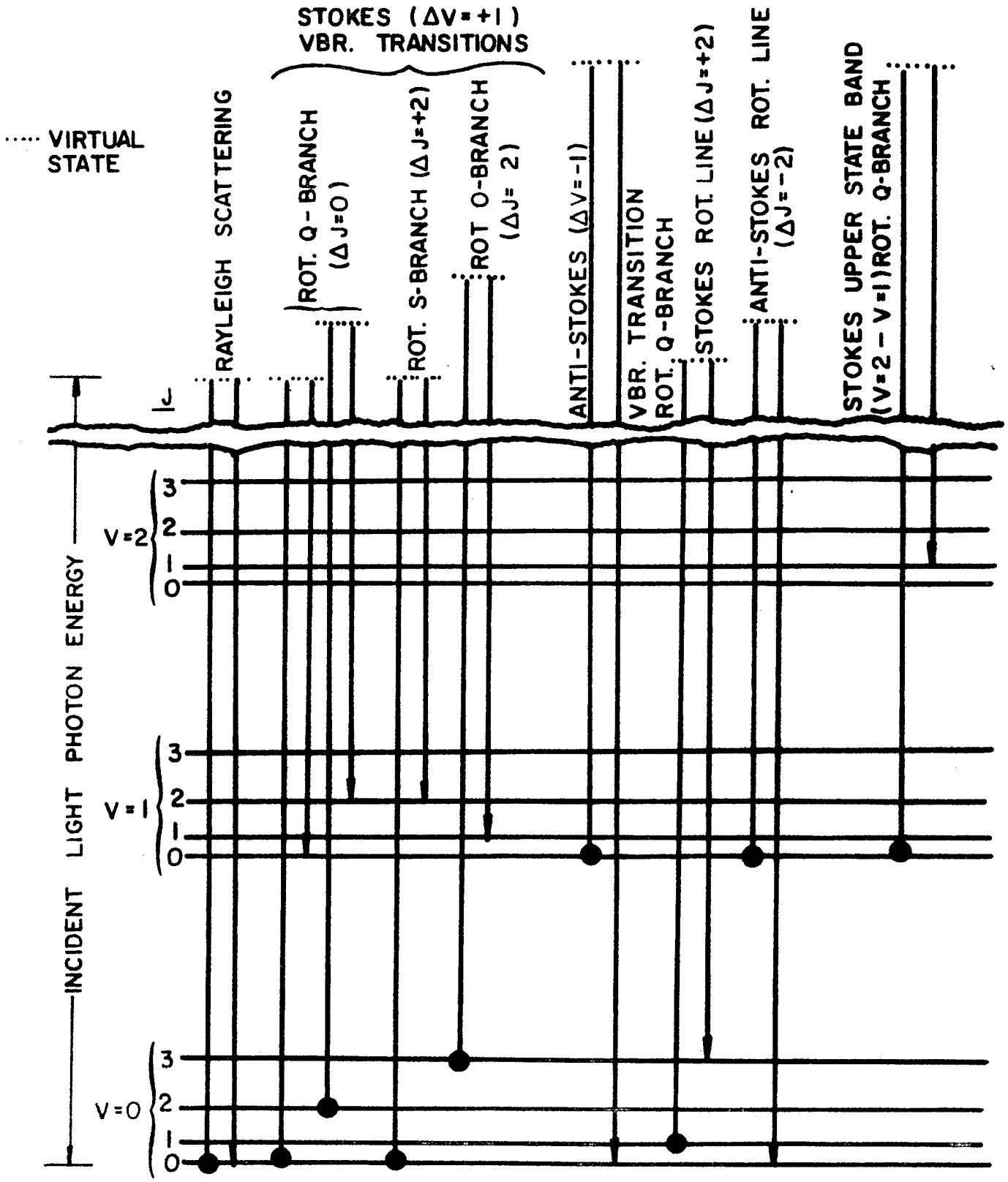


FIG. 1 SCHEMATIC DIAGRAM OF MOLECULAR TRANSITIONS

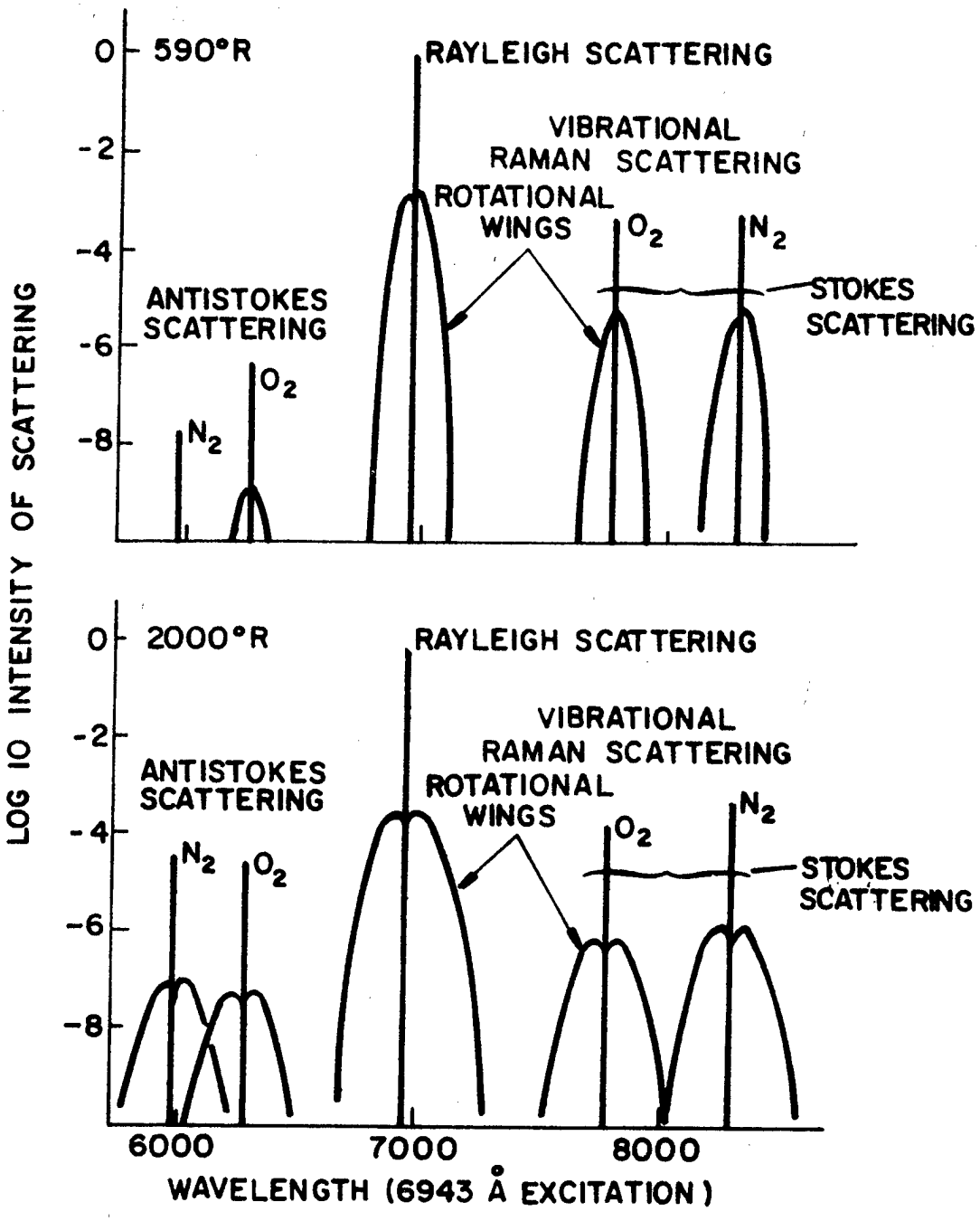


FIG. 2 RAMAN AND RAYLEIGH SCATTERING FROM AIR

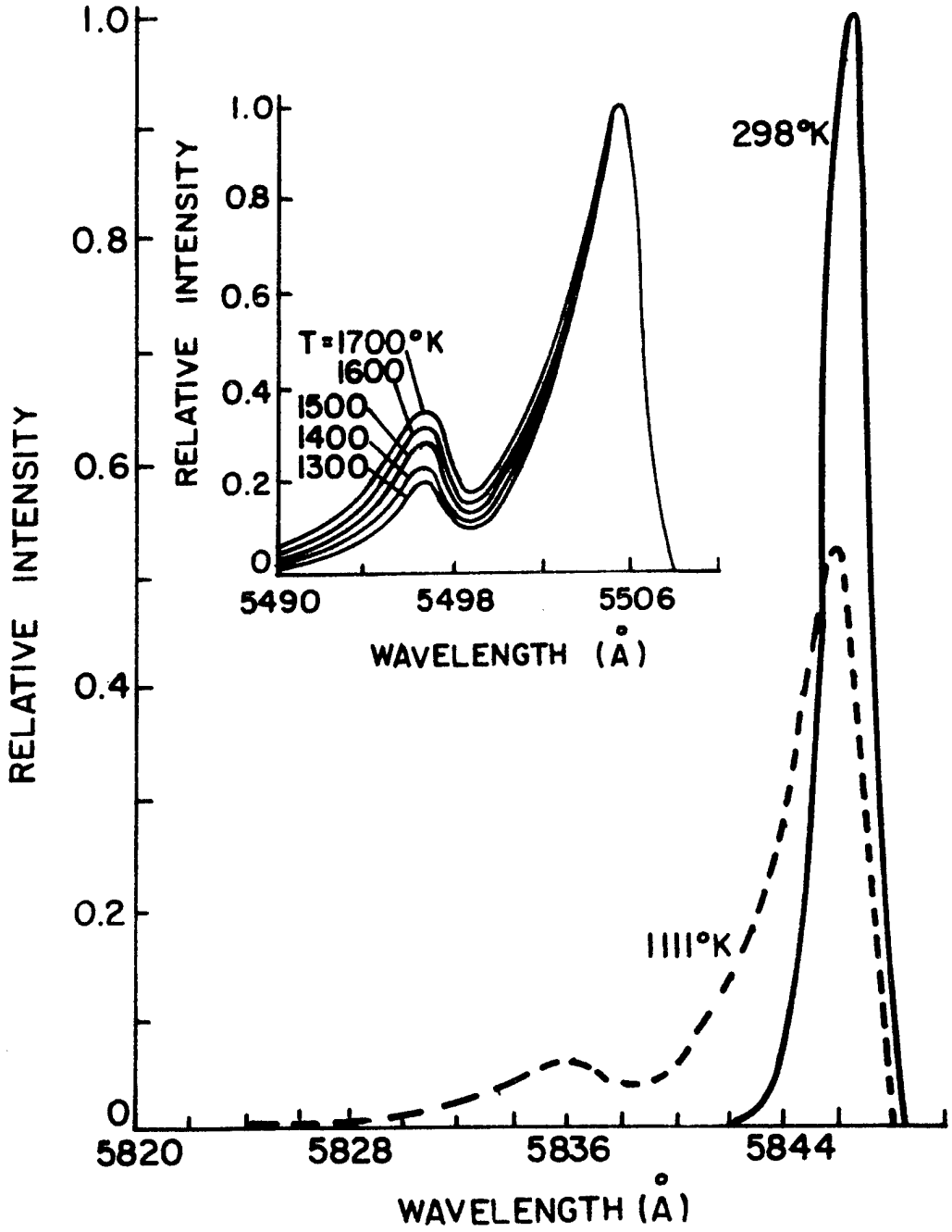


FIG. 3 THE RESOLVED Q-BRANCH

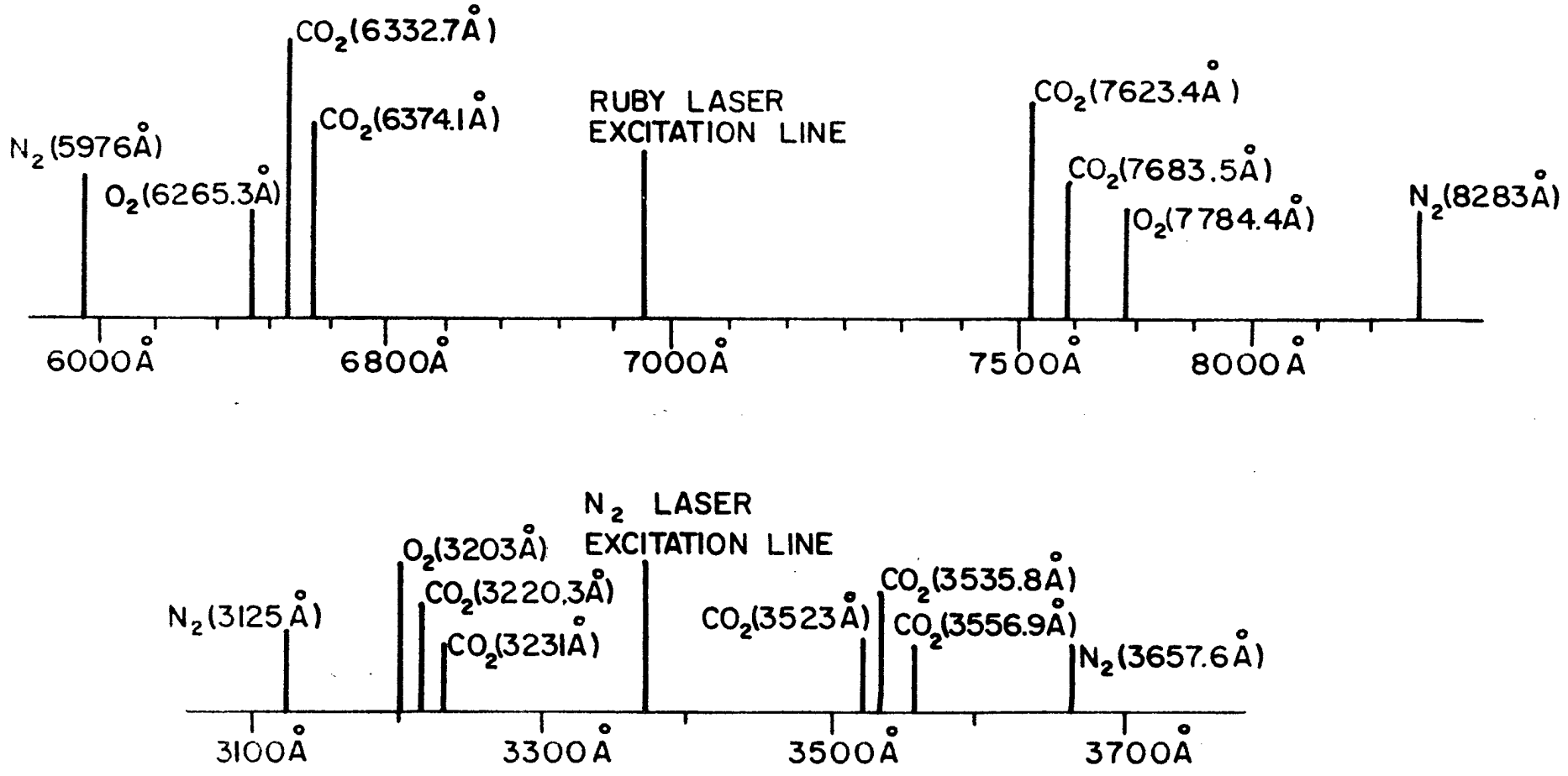


FIG. 4 VIBRATIONAL LINE DENSITY AS A FUNCTION OF 3 GASES

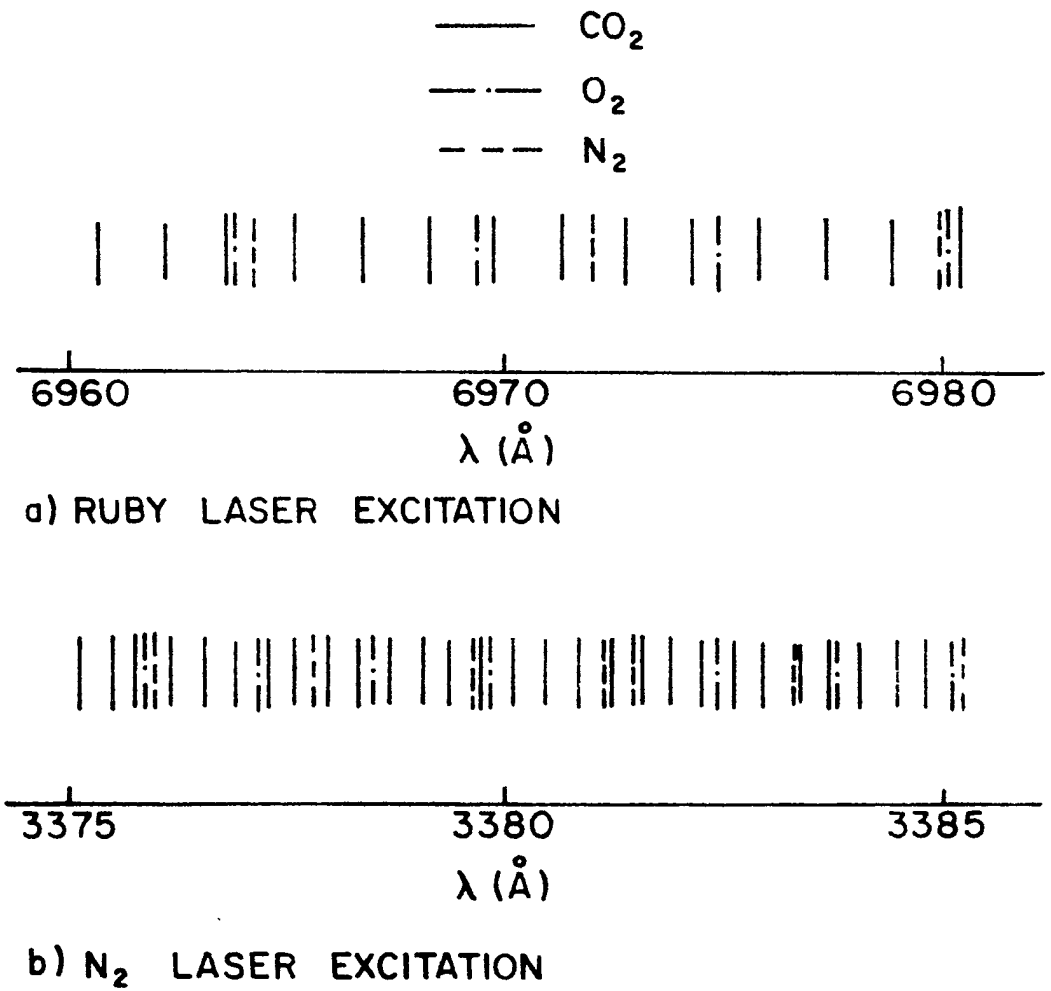


FIG. 5 ROTATIONAL LINE DENSITY OF A MIXTURE OF 3 GASES

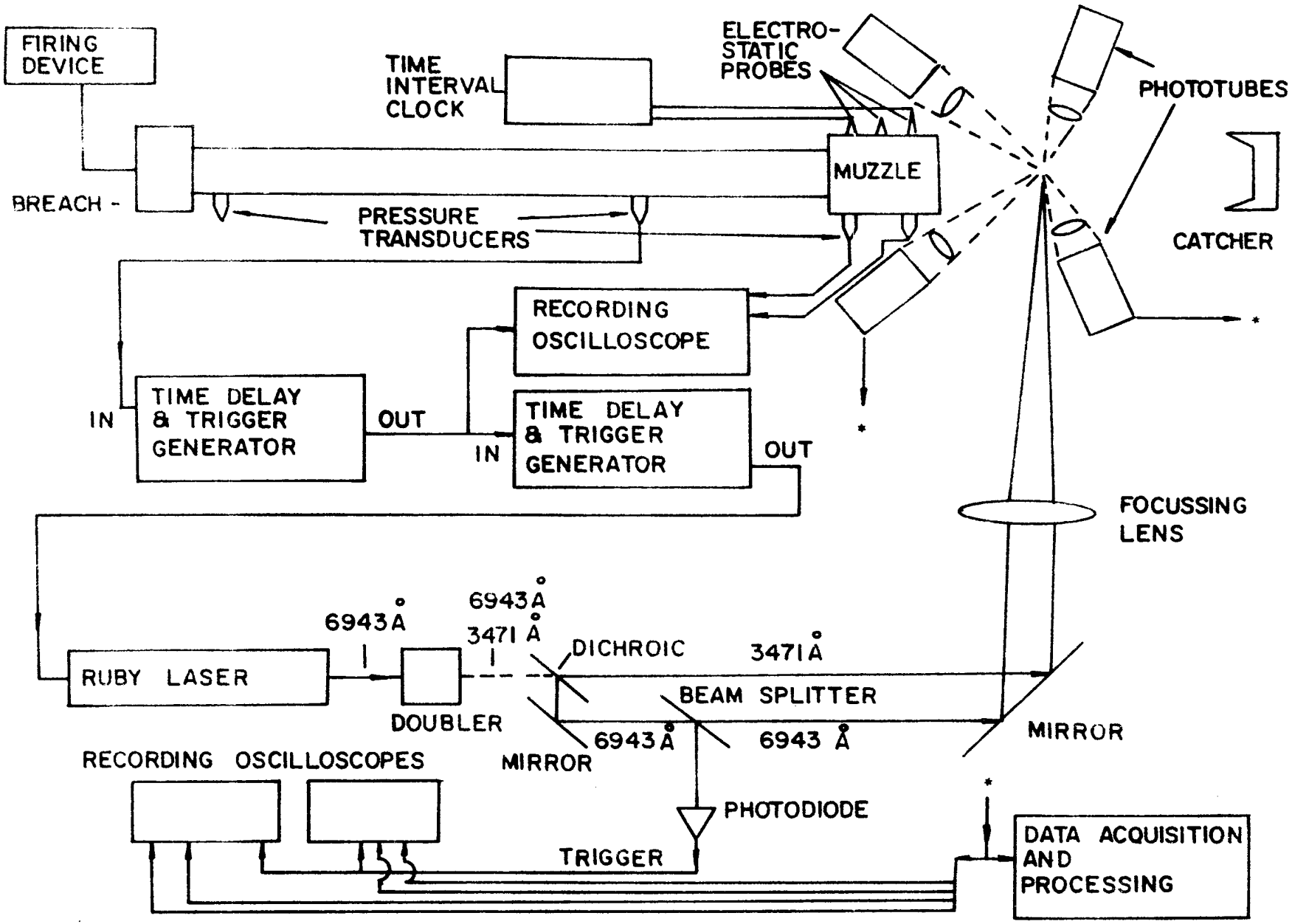


FIG. 6 SCHEMATIC DIAGRAM OF EXPERIMENTAL CONFIGURATION

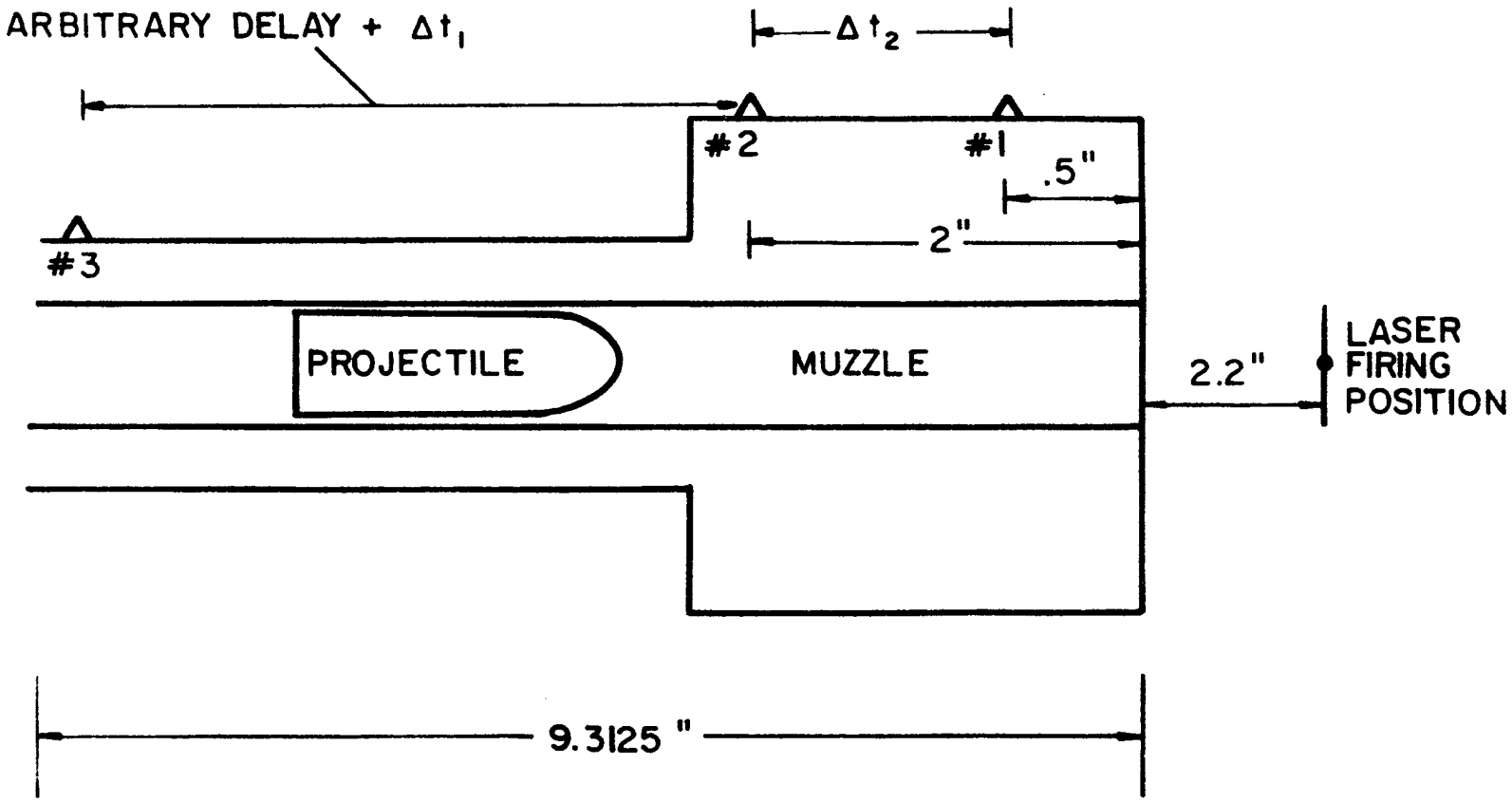
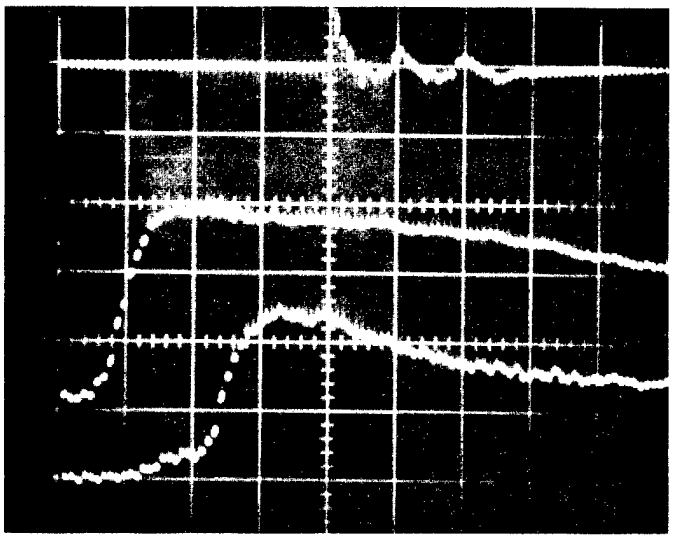
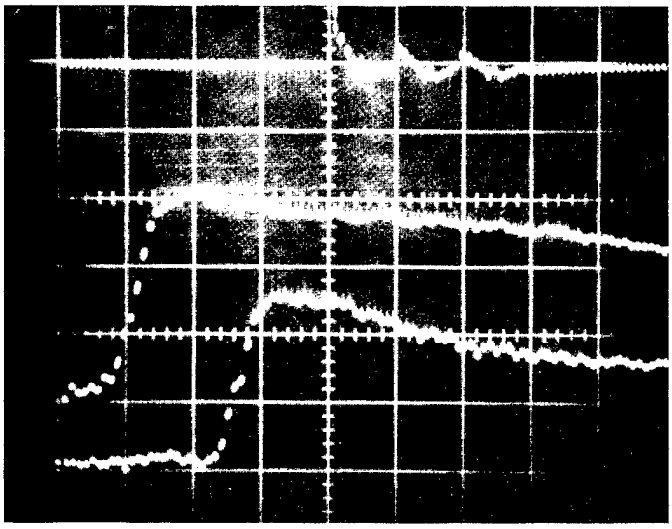


FIG. 7 GUN BARREL PRESSURE INSTRUMENTATION

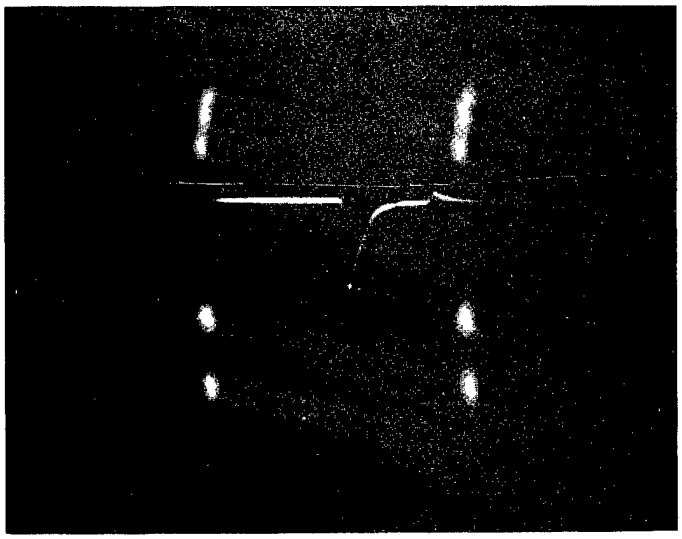


TEST # 210

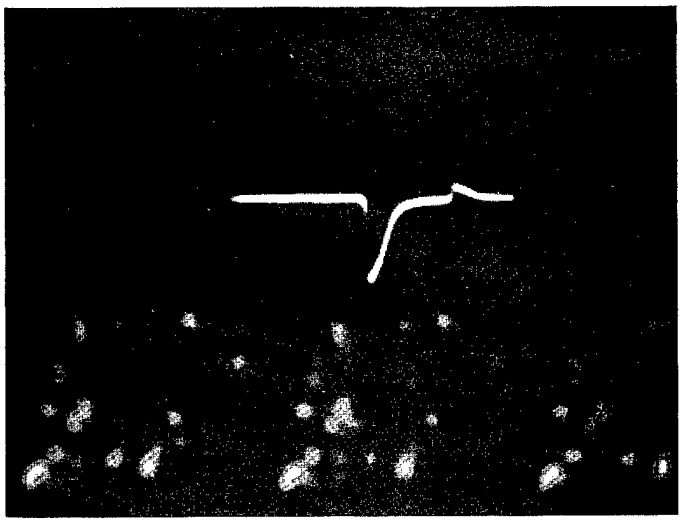


TEST # 211

FIG. 8 TEST DATA

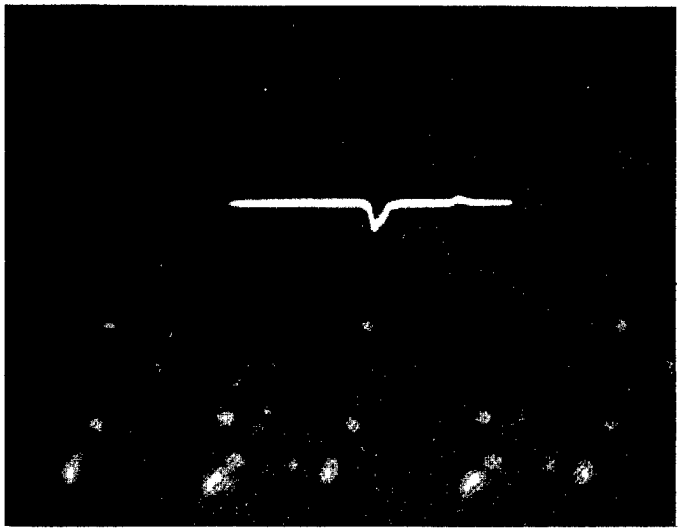


ANTI-STOKES



STOKES

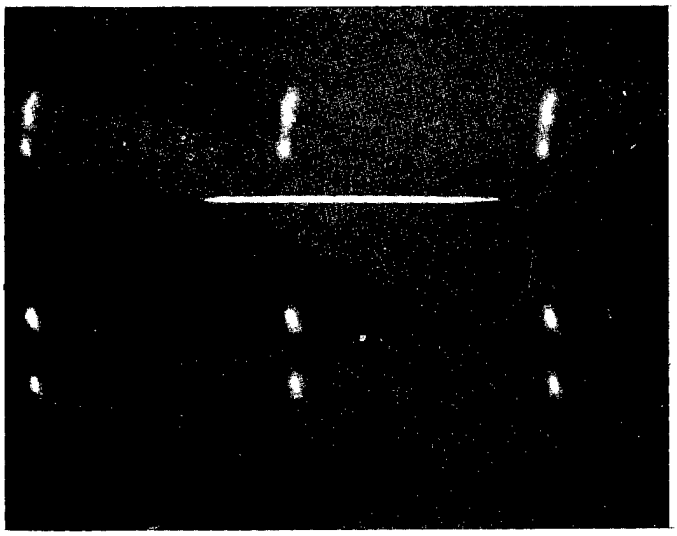
FIG. 9 STOKES AND ANTI-STOKES DATA FOR A TYPICAL TEST



STOKES

ANTI-STOKES

FIG. 10 STOKES AND ANTI-STOKES DATA FOR ATMOSPHERIC NITROGEN



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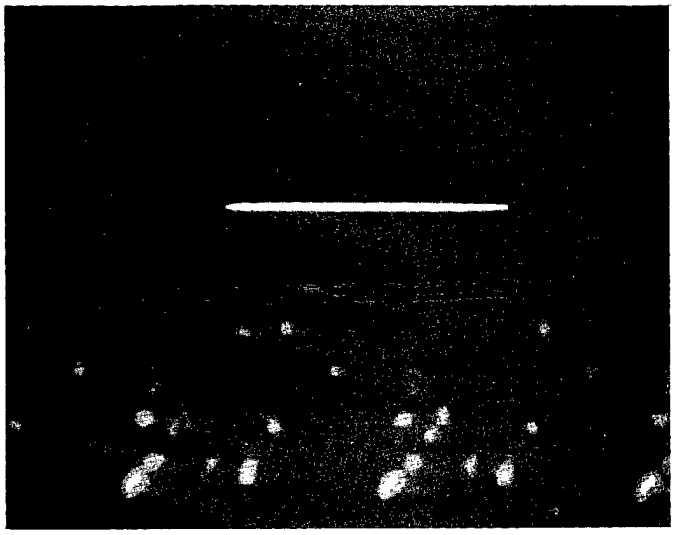

STOKES

FIG. 11 STOKES AND ANTI-STOKES DATA FROM MUZZLE FLASH

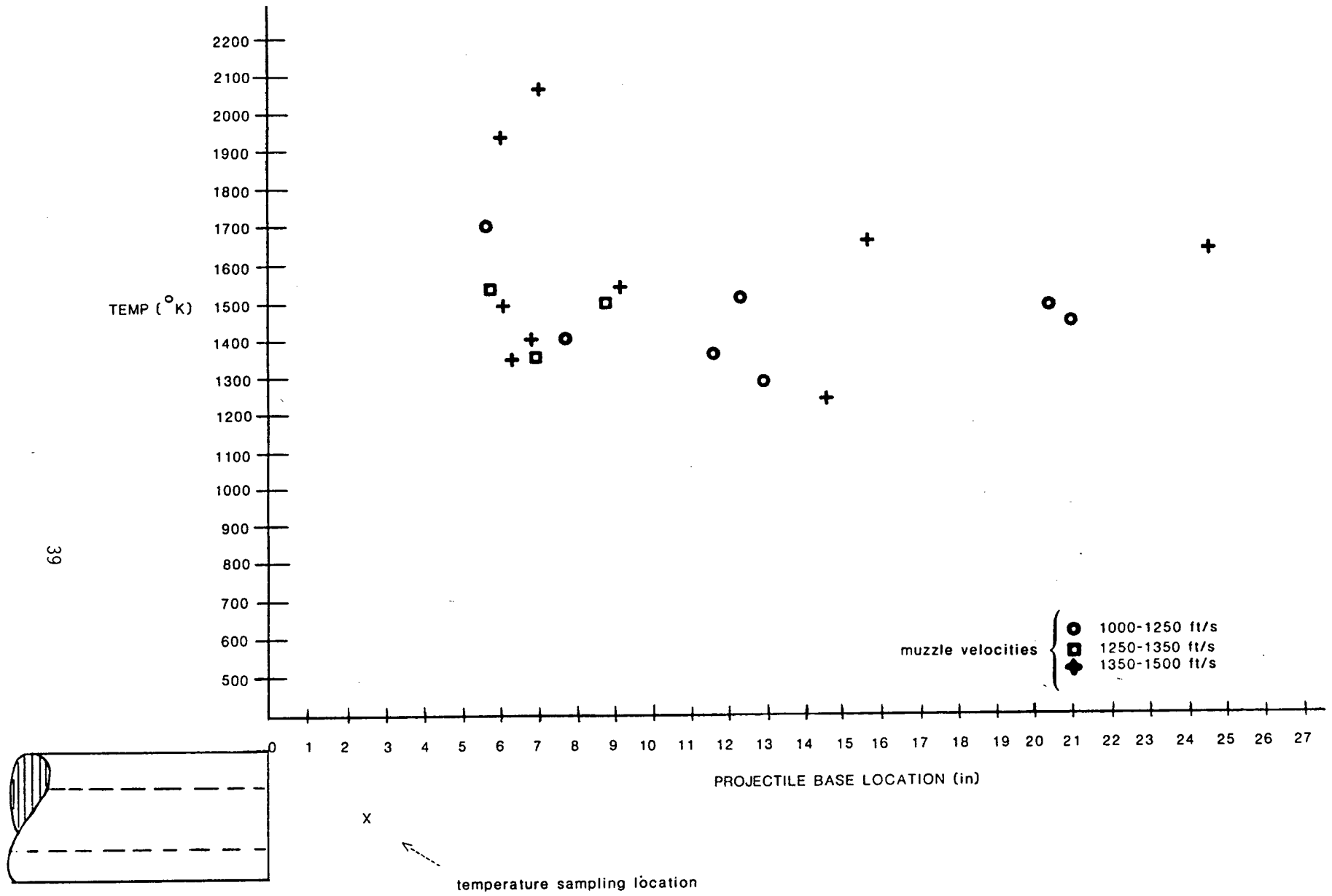

FIG.(12) MEASURED TEMPERATURES AT MUZZLE OF 20 mm GUN

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